

LM1042 Fluid Level Detector

The LM1042 uses the thermal-resistive probe technique to measure the level of non-flammable fluids. An output is pro-

vided proportional to fluid level and single shot or repeating

measurements may be made. All supervisory requirements

to control the thermal-resistive probe, including short and

open circuit probe detection, are incorporated within the de-

vice. A second linear input for alternative sensor signals

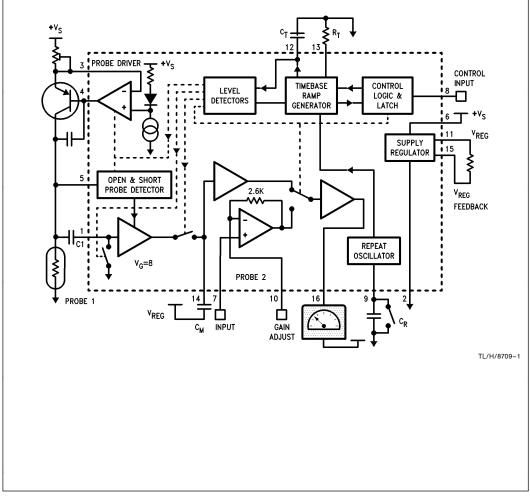
General Description

Features

- Selectable thermal-resistance or linear probe inputs
- Control circuitry for thermal-resistive probe
- Single-shot or repeating measurements
- Switch on reset and delay to avoid transients
- Output amplifier with 10 mA source and sink capability
- Short or open probe detection
- \blacksquare +50V transient protection on supply and control input
- 7.5V to 18V supply range
- Internally regulated supply
- -40°C to +80°C operation

Block Diagram

may also be selected.



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If Military/Aerospace specified devices are re	quired,	Output Current Pin 11 (source)	25 mA
please contact the National Semiconductor		Output Current Pin 16	\pm 10 mA
Office/Distributors for availability and specificat		Operating Temperature Range	-40°C to +80°C
Supply Voltage V _{CC}	32V	Storage Temperature Range	-55°C to +150°C
Voltage at Pin 8	32V	Lead Temperature (Soldering 10 sec.)	260°C
Positive Peak Voltage (Pins 6, 8, 3) (Note 1) 10 ms 2A	50V	Package Power Dissipation $T_A = 25^{\circ}C$ (Note 8)	1.8W
Output Current Pin 4, (I ₄)(sink)	10 mA	Device Power Dissipation	0.9W

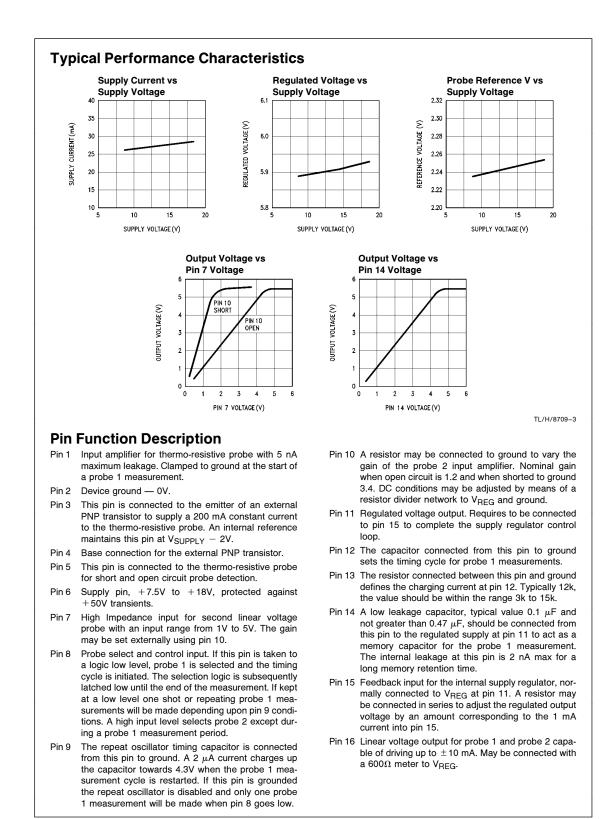
Electrical Characteristics

 V_{CC} = 13V, T_A within operating range except where stated otherwise. C_T = 22 $\mu F,\,R_T$ = 12k

Symbol	Parameter	Conditions	Tested Limits (Note 2)		Design Limits (Note 3)			Units
-			Min	Max	Min	Тур	Max	
V _{CC}	Supply Voltage		7.5	18	7.5	13	18	V
IS	Supply Current			35			35	mA
V _{REG}	Regulated Voltage	Pins 15 and 11 connected	5.7	6.15	5.65	5.9	6.2	V
	Stability Over V_{CC} Range	Referred to value at $V_{CC} = 13V$ (Note 4)		±0.5			±0.5	%
V ₆ -V ₃	Probe Current Reference Voltage		2.15	2.35	2.10	2.25	2.40	v
	Probe Current Regulation Over V _{CC} Range	(Note 4)		±0.5			±0.8	%
T ₁	Ramp Timing	See <i>Figure 5</i>	20	37	15	31	42	ms
$T_2 - T_1$					3		16	ms
$T_4 - T_1$	Ramp Timing		1.4	2.1	1.4	1.75	2.1	s
T _{STAB}	Ramp Timing Stability	Over V _{CC} Range		+5			±5	%
R _T	Ramp Resistor Range		3	15	3		15.0	kΩ
V ₈	Start Input Logic High Level		1.7		1.7			V
V ₈	Start Input Logic Low Level			0.5			0.5	V
l ₈	Start Input Current	$V_8 = V_{CC}$		100			100	nA
I ₈	Start Input Current	$V_8 = 0V$		300			300	nA
V ₁₆	Maximum Output Voltage	$R_L = 600\Omega$ from	V _{REG} -0.3		V _{REG} -0.3			V
	Minimum Output Voltage	Pin 16 to V _{REG}		0.5		0.2	0.6	V
G ₁	PROBE 1 Probe 1 Gain	Pin 1 80 mV to 520 mV (Notes 6, 7)	9.9	10.4		10.15		
	Non-linearity of G ₁	(Notes 0, 7) Pin 1 80 mV to 520 mV (Note 7)	-1	+ 1	-2	0	2	%
OS ₁	Pin 1 Offset	(Note 7)				±5		mV
G ₂	PROBE 2 Probe 2 Gain	Pin 7 240 mV to 1.562V (Note 7)	3.31	3.49		3.4		
	Non-linearity of G ₂	Pin 7 240 mV to 1.562V (Note 7)	-1	+1	-2	0.2	2	%
OS ₇	Pin 7 Offset	(Note 7)				±5		mV
R ₇	Input impedance					5		MΩ

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Symbol	Parameter	Conditions	Tested Limits (Note 2)		Design Limits (Note 3)			
			Min	Max	Min	Тур	Max	Unite
V ₁	Probe 1 Input Voltage Range	$\label{eq:V_CC} \begin{array}{l} V_{CC} = 9V \mbox{ to } 18V \\ V_{CC} = 7.5V, \mbox{ I}_4 < 2.5 \mbox{ mA} \\ (V_{REG} = 6.0V) \end{array}$	1	5	1 1		5 3.5	V V
V ₅	Probe 1 Open Circuit Threshold	At Pin 5	V _{REG} -0.7	V _{REG} -0.5	V _{REG} -0.85	V _{REG} -0.6	V _{REG} -0.35	v
V5	Probe 1 Short Circuit Threshold		0.5	0.7	0.35	0.6	0.85	v
I ₁₄	Pin 14 Input Leakage Current	Pin 14 = 4V	-2.0	2.0			2.0	nA
I ₁	Pin 1 Input Leakage Current	Pin 1 = 300 mV	-5.0	5.0		1.5	5.0	nA
T _R	Repeat Period	$C_{R} = 22 \ \mu F$ (Note 5)	12	28	9.1	17	36	s
	C _R Discharge Time	$C_{R} = 22 \ \mu F$				70	135	ms
С _М	Memory Capacitor Value						0.47	μF
C ₁	Input Capacitor Value						0.47	μF
		+50V			11042	L/LL/0700_0		
Note 3: figures. Note 4: Note 5: Note 6: 4.1V to	Limits guardbanded to include p Variations over temperature ran Time for first repeat period, see Probe 1 amplifier tests are meas simulate ramp action. See Figure When measuring gain separate	$5000 \mu F$ $0V \bullet I$ on tested at 25°C. These limits are arametric variations. $T_A = -40^{\circ}C$ ge are not production tested. <i>Figure 6.</i> urred with pin 12 ramp voltage held a 5. ground wire sensing is required at	e used to calcul to +80°C and I between the T; pin 2 to ensure	ate outgoing qu from $V_{CC} = 7.5$ $_3$ and T_4 condition	Ti ality levels. SV to 18V. These ons (pin 12 \approx 1.1 curate results.			
Note 3: figures. Note 4: Note 5: Note 6: 4.1V to Note 7:	Limits guardbanded to include p Variations over temperature ran Time for first repeat period, see Probe 1 amplifier tests are meas simulate ramp action. See Figure When measuring gain separate	$6000 \mu F$ 0V on tested at 25°C. These limits are arametric variations. $T_A = -40^{\circ}C$ ge are not production tested. <i>Figure 6.</i> ured with pin 12 ramp voltage helds a 5. ground wire sensing is required at ence between the predicted value	e used to calcul to +80°C and I between the T; pin 2 to ensure	ate outgoing qu from $V_{CC} = 7.5$ $_3$ and T_4 condition	Ti ality levels. SV to 18V. These ons (pin 12 \approx 1.1 curate results.	limits are not us		



Application Notes

THERMO-RESISTIVE PROBES — OPERATION AND CONSTRUCTION

These probes work on the principle that when power is dissipated within the probe, the rise in probe temperature is dependent on the thermal resistance of the surrounding material and as air and other gases are much less efficient conductors of heat than liquids such as water and oil it is possible to obtain a measurement of the depth of immersion of such a probe in a liquid medium. This principle is illustrated in *Figure 1*.

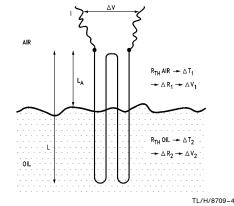


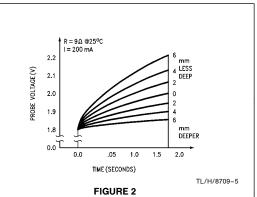
FIGURE 1

During the measurement period a constant current drive I is applied to the probe and the voltage across the probe is sampled both at the start and just before the end of the measurement period to give $\Delta V.$ R_{TH} Air and R_{TH} Oil represent the different thermal resistances from probe to ambient in air or oil giving rise fo temperature changes ΔT_1 and ΔT_2 respectively. As a result of these temperature changes the probe resistance will change by ΔR_1 or ΔR_2 and give corresponding voltage changes ΔV_1 or ΔV_2 per unit length. Hence

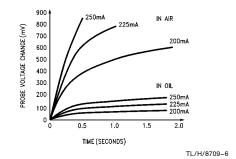
$$\Delta V = \frac{L_A}{L} \Delta V_1 + \frac{(L - L_A)}{L} \Delta V_2$$

and for $\Delta V_1 > \Delta V_2,$ R_{TH} Air > R_{TH} Oil, ΔV will increase as the probe length in air increases. For best results the probe needs to have a high temperature coefficient and low thermal time constant. One way to achieve this is to make use of resistance wires held in a suitable support frame allowing free liquid access. Nickel cobalt iron allov resistance wires are available with resistivity 50 $\mu\Omega \text{cm}$ and 3300 ppm temperature coefficient which when made up into a probe with 4 imes 2 cm 0.08 mm diameter strands between supports (10 cm total) can give the voltage vs time curve shown in Figure 2 for 200 mA probe current. The effect of varying the probe current is shown in Figure 3. To avoid triggering the probe failure detection circuits the probe voltage must be between 0.7V and 5.3V (V_{REG} - 6V), hence for 200 mA the permissible probe resistance range is from 3.5Ω to 24Ω . The example given has a resistance at room temperature of 9Ω which leaves plenty of room for increase during measurements and changes in ambient temperature.

Various arrangements of probe wire are possible for any given wire gauge and probe current to suit the measurement range required, some examples are illustrated schematically in *Figure 4.* Naturally it is necessary to reduce the probe

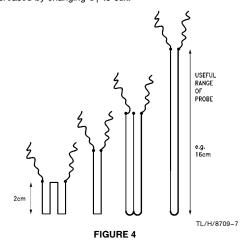


current with very fine wires to avoid excessive heating and this current may be optimized to suit a particular type of wire. The temperature changes involved will give rise to noticeable length changes in the wire used and more sophisticated holders with tensioning devices may be devised to allow for this.





Probes need not be limited to resistance wire types as any device with a positive temperature coefficient and sufficiently low thermal resistance to the encapsulation so as not to mask the change due to the different surrounding mediums, could be used. Positive temperature coefficient thermistors are a possibility and while their thermal time constant is likely to be longer than wire the measurement time may be increased by changing C_T to suit.

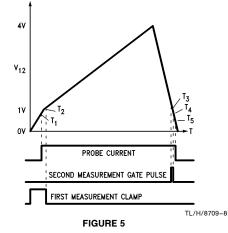


Application Notes (Continued)

CIRCUIT OPERATION

1) Thermo-Resistive Probes

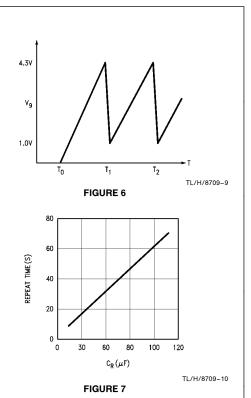
These probes require measurements to be made of their resistance before and after power has been dissipated in them. With a probe connected as probe 1 in the connection diagram the LM1042 will start a measurement when pin 8 is taken to a logic low level (V_8 < 0.5V) and the internal timebase ramp generator will start to generate the waveform shown in Figure 5. At 0.7V, T1, the probe current drive is switched on supplying a constant 200 mA via the external PNP transistor and the probe failure circuit is enabled. At 1V pin 1 is unclamped and $\ensuremath{C_1}$ stores the probe voltage corresponding to this time, T2. The ramp charge rate is now reduced as CT charges toward 4V. As the 4.1V threshold is passed a current sink is enabled and CT now discharges. Between 1.3V and 1.0V, T_3 and T_4 , the amplified pin 1 voltage, representing the change in probe voltage since T₂ (and as the current is constant this is proportional to the resistance change) is gated onto the memory capacitor at pin 14. At 0.7V, T₅, the probe current is switched off and the measurement cycle is complete. In the event of a faulty probe being detected the memory capacitor is connected to the regulated supply during the gate period. The device leakage at pin 14 is a maximum of 2 nA to give a long memory retention time. The voltage present on pin 14 is amplifed by 1.2 to drive pin 16 with a low impedance, $\pm\,10$ mA capability, between 0.5V and 4.7V. A new measurement can only be started by taking pin 8 to a low level again or by means of the repeat oscillator.



2) Repetitive Measurement

With a capacitor connected between pin 9 and ground the repeat oscillator will run with a waveform as shown in *Figure* δ and a thermo-resistive probe measurement will be triggered each time pin 9 reaches a threshold of 4.3V, provided pin 8 is at a logic low level. The repeat oscillator runs independently of the pin 8 control logic.

As the repetition rate is increased localized heating of the probe and liquid being measured will be the main consideration in determining the minimum acceptable measurement intervals. Measurements will tend to become more dependent on the amount of fluid movement changing the rate of heat transfer away from the probe. The typical repeat time versus timing capacitor value is shown in *Figure 7*.



3) Second Probe Input

A high impedance input for an alternative sensor is available at pin 7. The voltage applied to this input is amplified and output at pin 16 when the input is selected with a high level on pin 8. The gain is defined by the feedback arrangement shown in *Figure 8* with adjustment possible at pin 10. With pin 10 open the gain is set at a nominal value of 1.2, and this may be increased by connecting a resistor between pin 10 and ground up to a maximum of 3.4 with pin 10 directly grounded. A variable resistor may be used to calibrate for the variations in sensitivity of the sensor used for probe 2.

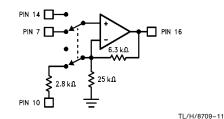
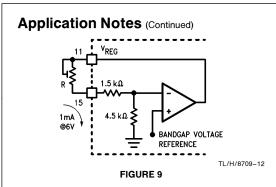


FIGURE 8

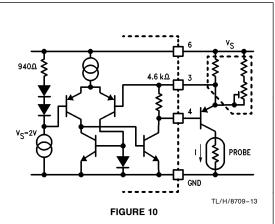
POWER SUPPLY REGULATOR

The arrangement of the feedback for the supply regulator is shown in *Figure 9.* The circuit acts to maintain pin 15 at a constant 6V and when directly connected to pin 11 the regulated output is held at 6V. If required a resistor R may be connected between pins 15 and 11 to increase the output voltage by an amount corresponding typically to 1 mA flowing in R. In this way a variable resistor may be used to trim out the production tolerance of the regulator by adjusting for V_{REG} $\geq 6.2V.$



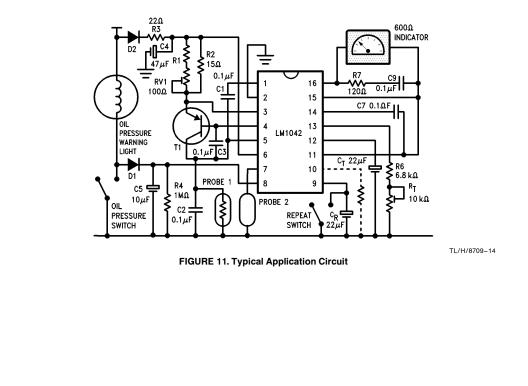
PROBE CURRENT REFERENCE CIRCUIT

The circuit defining the probe circuit is given in *Figure 10*. A reference voltage is obtained from a bandgap regulator derived current flowing in a diode resistor chain to set up a voltage 2 volts below the supply. This is applied to an amplifier driving an external PNP transistor to maintain pin 3 at 2V below supply. The emitter resistance from pin 3 to supply defines the current which, less the base current, flows in the probe. Because of the sensitivity of the measurement to probe current evident in *Figure 3* the current should be adjusted by means of a variable resistor to the desired value. This adjustment may also be used to take out probe tolerances.

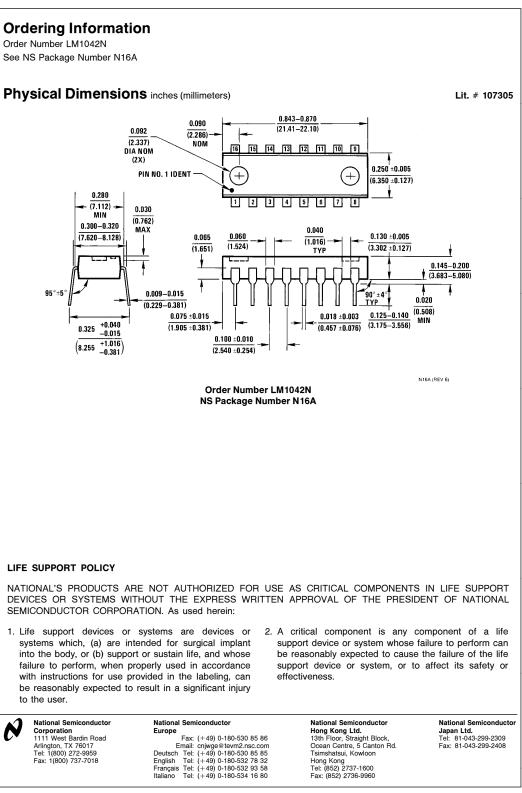


TYPICAL APPLICATIONS CIRCUIT

A typical automotive application circuit is shown in *Figure 11* where the probe selection signal is obtained from the oil pressure switch. At power up (ignition on) the oil pressure switch is closed and pin 8 is held low by R4 causing a probe 1 (oil level) measurement to be made. Once the engine has started the oil pressure switch opens and D1 pulls pin 8 high changing over to the second auxiliary probe input. The capacitor C₅ holds pin 8 high in the event of a stalled engine so that a second probe 1 measurement can not occur in disturbed oil. Non-automotive applications may drive pin 8 directly with a logic signal.



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